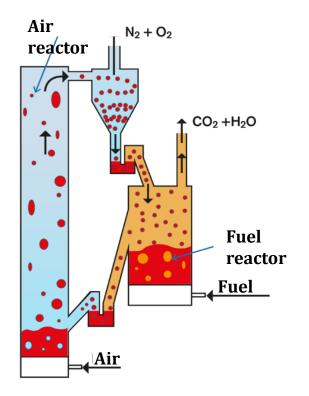
# **Chemical-Looping Combustion**

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# CO<sub>2</sub> capture at low cost and energy penalty



# Anders Lyngfelt

Net-zero Emission Technologies for Sustainable Development: Challenges and Opportunities N0ET – 2022 December 12-13 Dhanbad, India



#### **CONTENT**

- Negative CO<sub>2</sub> emissions through Bio-Energy CCS
  - Principle
  - Need
  - Incentivizing
- Chemical-Looping Combustion (CLC)
  - Principles
  - Pilot experience
  - Oxygen carrier
- CLC Applications
  - CLC of coal
  - CLC biomass
  - CLC for blue hydrogen
- Circulation
- Downstream treatment

# Removal of CO<sub>2</sub> from the atmosphere

# **Negative Emissions**

**Bio-CCS** 



Growing trees/plants remove CO<sub>2</sub> from the atmosphere.

**BUT,** the CO<sub>2</sub> can be prevented from returning:

Capture and storage of CO<sub>2</sub> from combustion of biomass/biowaste



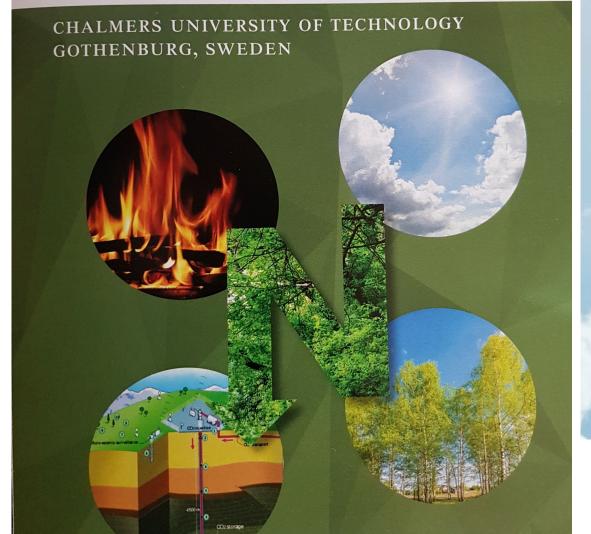
# **Bio-CCS (BECCS)**

(BioEnergy Carbon Capture and Storage)

INTERNATIONAL CONFERENCE ON

# NEGATIVE CO<sub>2</sub> EMISSIONS

MAY 22-24, 2018



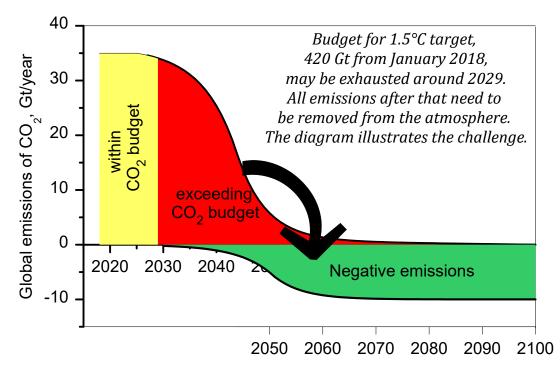


2<sup>ND</sup> INTERNATIONAL CONFERENCE ON

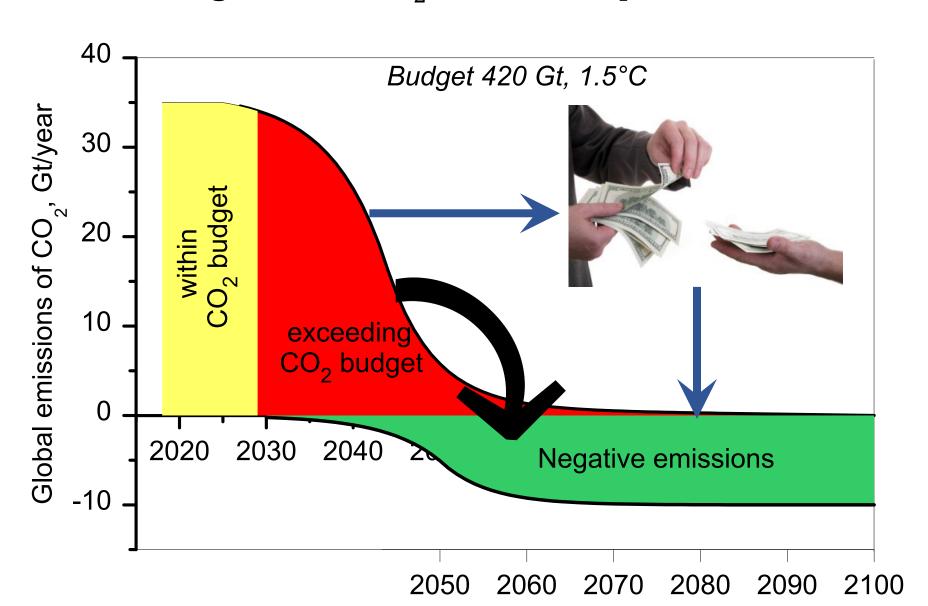
# NEGATIVE CO<sub>2</sub> EMISSIONS

JUNE 14-17, 2022

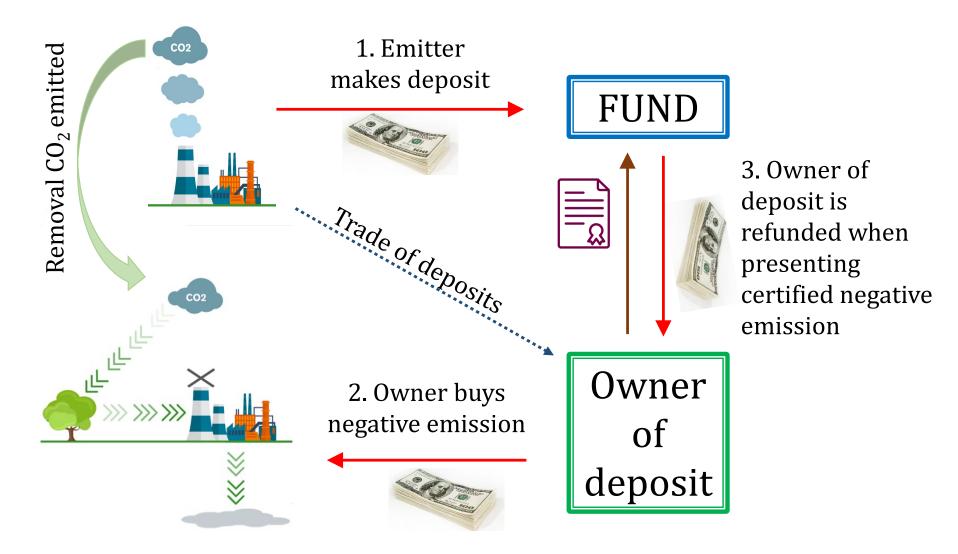
- Global carbon budget for +1.5°C likely spent around 2029
- Emission reductions cannot be made fast enough to meet the target
- To meet max 1.5°C, all CO<sub>2</sub> emissions after 2029 must be removed from the atmosphere.
- Enormous negative emissions needed to meet max 1.5°C,
- No realistic mechanism for financing of future negative emissions in place.



Proposal: Make emitters responsible for, i.e. pay for, removing emitted CO<sub>2</sub> from atmosphere



# **Atmospheric CO<sub>2</sub> Removal Deposits (ACORDs)**



Lyngfelt, Anders, and Fridahl, Mathias, CO<sub>2</sub> Emitter Liability using Atmospheric CO<sub>2</sub> Removal Deposits (ACORDs) for Financing of Future Negative Emissions, 2<sup>nd</sup> International Conference on Negative CO<sub>2</sub> Emissions, June 14-17, 2022, Göteborg, Sweden

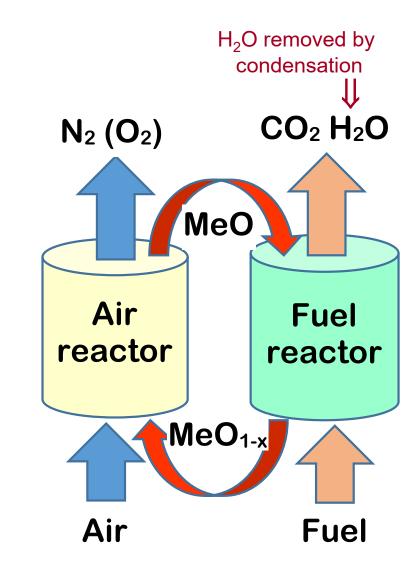
# **Chemical-Looping Combustion (CLC)**

Oxygen is transferred from air to fuel by metal oxide particles

Inherent CO<sub>2</sub> capture:

- fuel and combustion air *never mixed*
- no active gas separation needed

**Unique** potential for reducing costs of CO<sub>2</sub> capture!

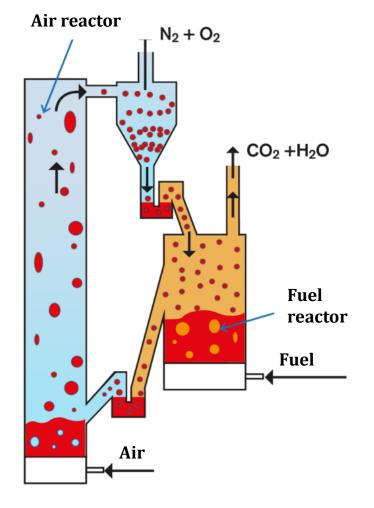


High similarity between Chemical Looping Combustion and Circulating Fluidized-Bed (CFB) boilers

Circulating fluidized-bed boiler (commonly used for solid fuels)



#### **Chemical Looping Combustion**



But, does it work in practice?

Yes, it works!!



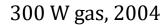
# Total chemical-looping operation at Chalmers: 4 200 h in four pilots



10 kW solid fuel, 2006

Worldwide: >12 000 h in >50 pilots





100 kW solid fuel, 2011

10 kW gas, 2003

# The <u>oxygen carrier</u> is the cornerstone of CLC, analogous to the red blood cells transferring oxygen in the body

The oxygen carrier is made up of metal oxide particles of size 0.1-0.3 mm.

Operational temperature in CLC is typically 900 – 1000°C

Oxides based on *nickel, copper, iron and manganese* have been successfully used in chemical-looping pilot operation.

Many combined oxides have also been used, e.g. manganese + calcium/iron/magnesium/silicon, and iron + titanium (ilmenite)

Both manufactured materials and low-cost materials, such as manganese ore, iron ore and ilmenite ore have been used.

Natural ores are well suited for ash-containing solid fuels, such as coal and biomass

Highly performing manufactured, such as calcium manganate, are suitable for ash-free gaseous fuels



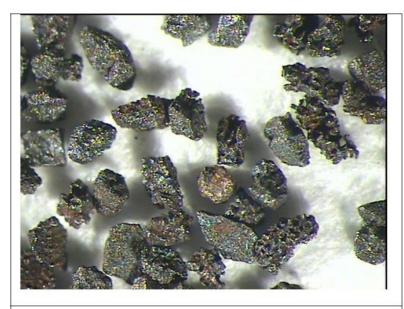


Figure 17 b. Used <u>Mangagran</u> particles, from AR. 180-212 μm.

#### Oxygen carriers continued

- >12 000 h of chemical-looping operation in smaller pilots:
- a significant number of materials that work well
- manufactured materials with high, even complete conversion
- low-cost natural minerals/industrial by-products
- sufficient reactivity and lifetime has been shown by a number of materials

>20 000 h of Oxygen Carrier Aided Combustion (OCAC) with ilmenite in CFB boilers, shows it can be used at industrial conditions

Lyngfelt, A., Chemical-Looping Combustion – Status and Development Challenges, Energy & Fuels 32 (2020) 9077-9093

Lind F., Corcoran A., Andersson B.-Å., and Thunman H., 12,000 Hours of Operation with Oxygen-Carriers in Industrially Relevant Scale (75,000 kWth), VGB Power TECH Journal, 7 (2017)

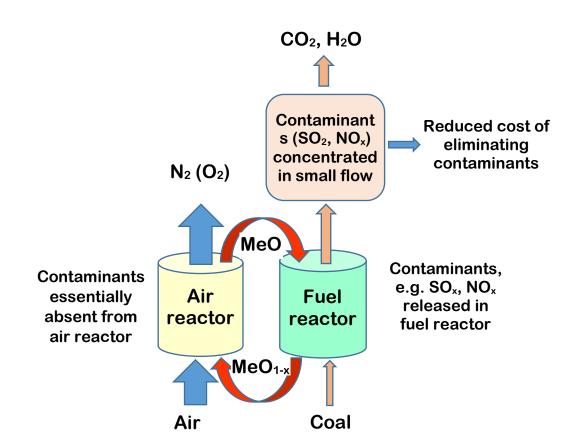
Moldenhauer, Patrick; Angelica Corcoran; Henrik Thunman and Fredrik Lind, A Scale-Up Project for Operating a 115 MWth Biomass-Fired CFB boiler with Oxygen Carriers as Bed Material, 5<sup>th</sup> International Conference on Chemical Looping, Park City, Utah, 24-27 September 2018

# Most important applications of CLC technology

- Coal combustion
- Biomass combustion
- Steam-Methane Reforming with Chemical-Looping Combustion (SMR-CLC)

# **Chemical-looping combustion of coal**

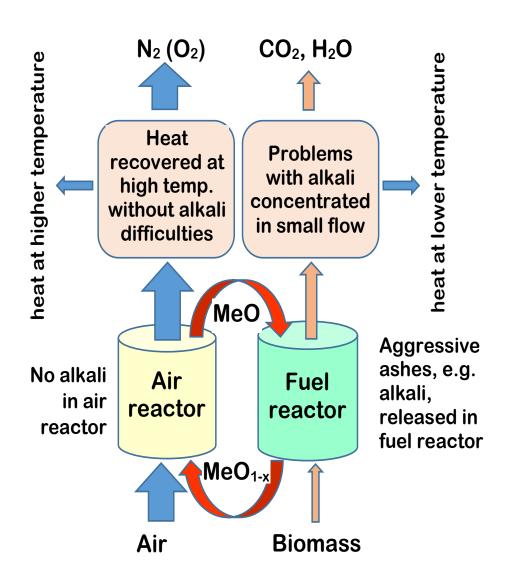
- high similarity to normal circulating fluidized bed technology
- small added cost, low energy penalty
- pollutants concentrated in CO<sub>2</sub> could reduce costs of SO<sub>x</sub>/NO<sub>x</sub> reduction
- unique potential for dramatic reduction in CO<sub>2</sub> capture cost
- large potential market



# **Chemical looping combustion of biomass**

- same advantages as in coal combustion above:
  - similarity to normal circulating fluidized bed technology
  - small added cost, low energy penalty
  - concentration of pollutants in CO<sub>2</sub>
  - unique potential for dramatic reduction in CO<sub>2</sub> capture cost
  - large potential market
- in addition potential advantage with respect to alkalis
- using biomass gives negative emissions
- to meet climate targets gigantic negative emissions are needed

#### **Chemical-looping combustion of biomass**



Alkali in biomass gives low ash-melting temperature together with silica (i.e. sand).

With ilmenite oxygen carrier (FeTiO<sub>3</sub>) the alkali forms **non-sticky** titanates.

>20,000 h of OCAC (oxygen-carrier aided combustion) in full-scale CFBs with ilmenite

Long-term operation with ilmenite, 300 h, shows alkali penetrates to centre of particles, and only minor loss in reactivity

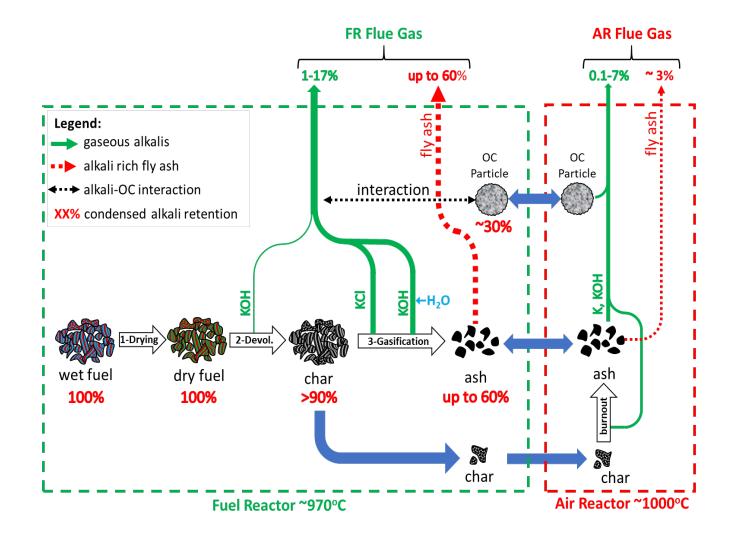
Only small part of alkali released in air reactor

Air reactor essentially free from chlorine

Could range of possible fuels be extended to more difficult fuels? (straw)

Studies of alkali flows in three CLC pilots found:

- majority of alkali retained in oxygen carrier
- majority of alkali in fly ash, from fuel reactor
- low fraction of alkali in air reactor outlet
- air reactor will be essentially free of KCl



Ivan Gogolev, Amir H. Soleimani Salim, Daofeng Mei and Anders Lyngfelt, Effects of Temperature, Operation Mode, and Steam Concentration on Alkali Release in Chemical Looping Conversion of Biomass – Experimental Investigation in a 10 kWth Pilot, Energy & Fuels, 36:17 (2022) 9551–9570

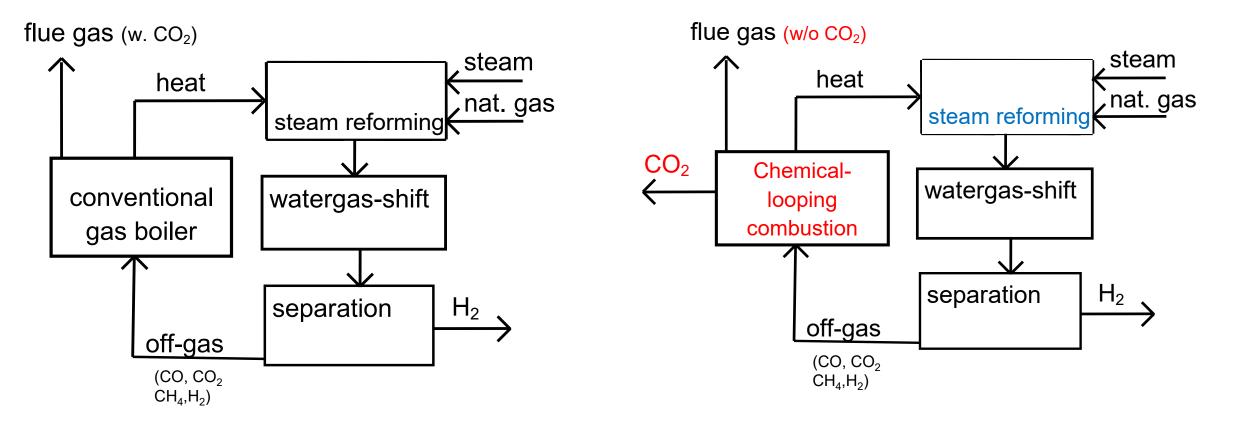
Ivan Gogolev, The Release, Distribution, and Implications of Alkalis in Chemical Looping Combustion of Biomass, PhD Thesis, Chalmers University of Technology, Göteborg, Sweden 2022

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## Blue hydrogen at low cost with CLC-SMR

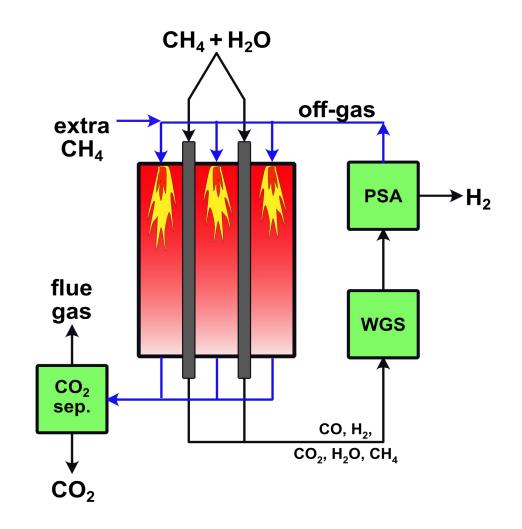
# **Steam methane reforming (SMR)**

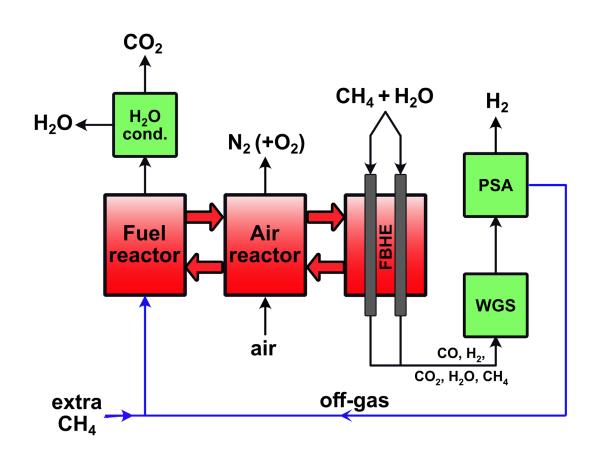
## **Steam reforming with CLC**



# **Steam Methane Reforming (SMR)**

# **Steam reforming with CLC**





# Why CLC-SMR?

Capture of CO<sub>2</sub> with no/small energy penalty

Negative energy penalty for process<sup>1</sup> (T outlet reduced from e.g. 1200 – 950°C)

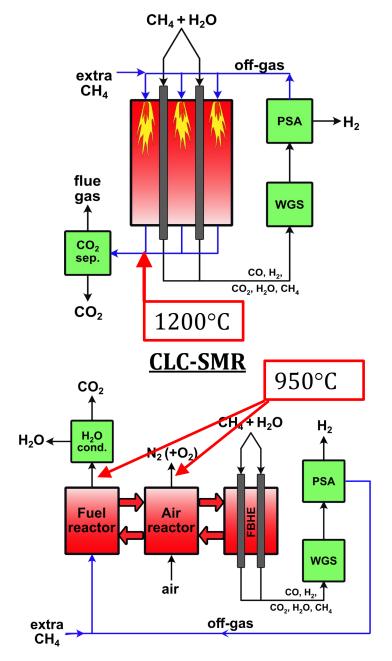
Capture of CO<sub>2</sub> with without high equipment/operational cost for gas separation

More efficient heat transfer and more benign conditions

- smaller tube diameter possible in FBHEs (fluidized-bed heat exchangers)
- thus, shorter and thinner tubes (length decrease by factor 3?)<sup>2</sup>
- thus, less catalyst (amount decreased by factor of 3?)<sup>2</sup>
- thus, lower cost of reforming step

In total: Potential for transforming natural gas to  $CO_2$ -free  $H_2$  with <u>negative</u> energy penalty and <u>negative</u> cost penalty for  $CO_2$  capture. Gigantic potential future market.

#### **Steam Methane Reforming (SMR)**



<sup>1)</sup> Stenberg V, Spallina V, Mattisson T, Rydén M. Techno-economic analysis of H<sub>2</sub> production processes using fluidized bed heat exchangers with steam reforming – Part 2: Chemical-looping combustion. *International Journal of Hydrogen Energy* **46** (2021) 25355-25375

<sup>2)</sup> Pröll, T., and Lyngfelt, A., Steam Methane Reforming with Chemical-Looping Combustion – Scaling of Fluidized Bed-Heated Reformer Tubes, *Energy & Fuels* 36:17 (2022) 9502–9512

#### **Commercial CLC plant**

Three critical aspects that must have adequate solution

1) An oxygen carrier that works  $\square$ 

2) Adequate circulation

3) Downstream treatment of gas from fuel reactor to achieve a  ${\rm CO_2}$  that fulfills purity requirements for transportation/ storage

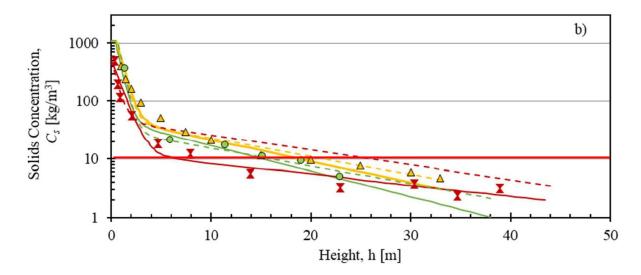
# 2) What is the circulation in commercial CFBs?

Upwards flow proportial to solids concentration  $\rho_s$  (kg/m3)

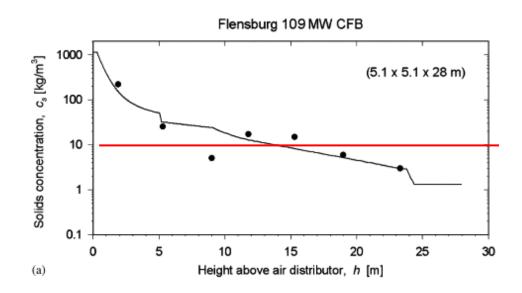
$$G_s = \rho_s(u_0 - u_s)$$

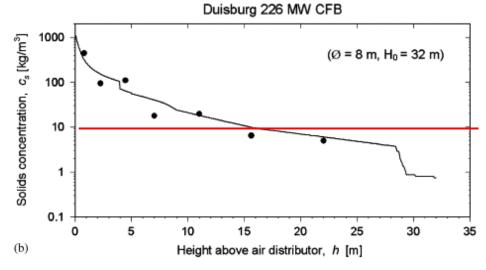
Needed circulation for Chemical-Looping Combustion needs:

$$\rho_s \ge 10 \text{ kg/m}^3$$



Solids concentration versus height for 3 CFB boilers. ▲ Emile Huchet, • Zibo, ▼ Turow.





Solids concentration versus height. Data from two CFB boilers

### **Conclusions**

Actual circulation in CFB boilers is 5-50% of what is needed for CLC

Raised gas velocity not an option due to damage to boiler walls.

With smaller particle size, upwards flow can be dramatically increased. But will the actual circulation also increase? Increased loss in cyclone?

As noted, upwards flow decreases exponentially with height.

However, collection of down-flow along the walls, would be sufficient.

Lyngfelt, A., Pallarés, D., Linderholm, C., Lind, F., Thunman, H., and Leckner, B., Achieving Adequate Circulation in Chemical-Looping Combustion – Design Proposal for a 200 MW<sub>th</sub> CLC Boiler, *Energy & Fuels* 36:17 (2022) 9588–9615

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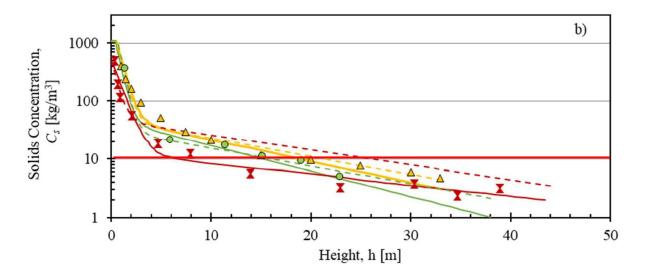
# 2) But upwards flow in lower part is sufficient

Upwards flow proportial to solids concentration (kg/m3)

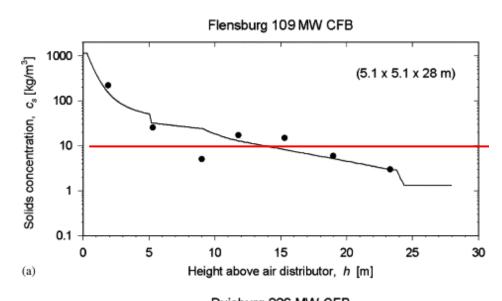
$$G_s = \rho_s(u_0 - u_s)$$

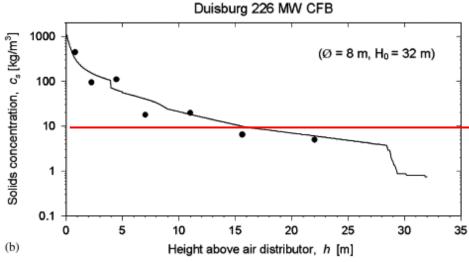
Needed circulation for Chemical-Looping Combustion needs:

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Solids concentration versus height for 3 CFB boilers. ▲ Emile Huchet, • Zibo, ▼ Turow.

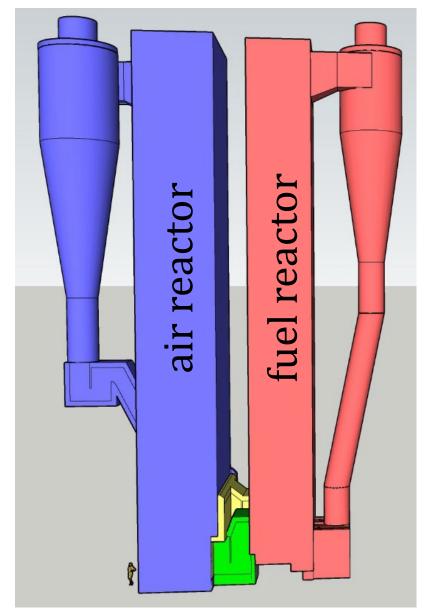


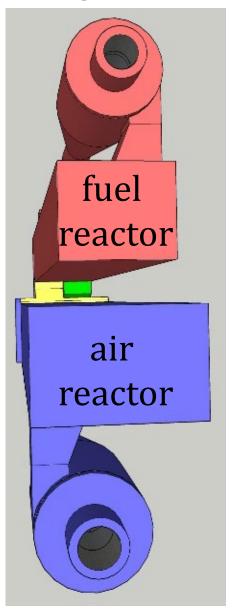


Solids concentration versus height.

Data from two CFB boilers

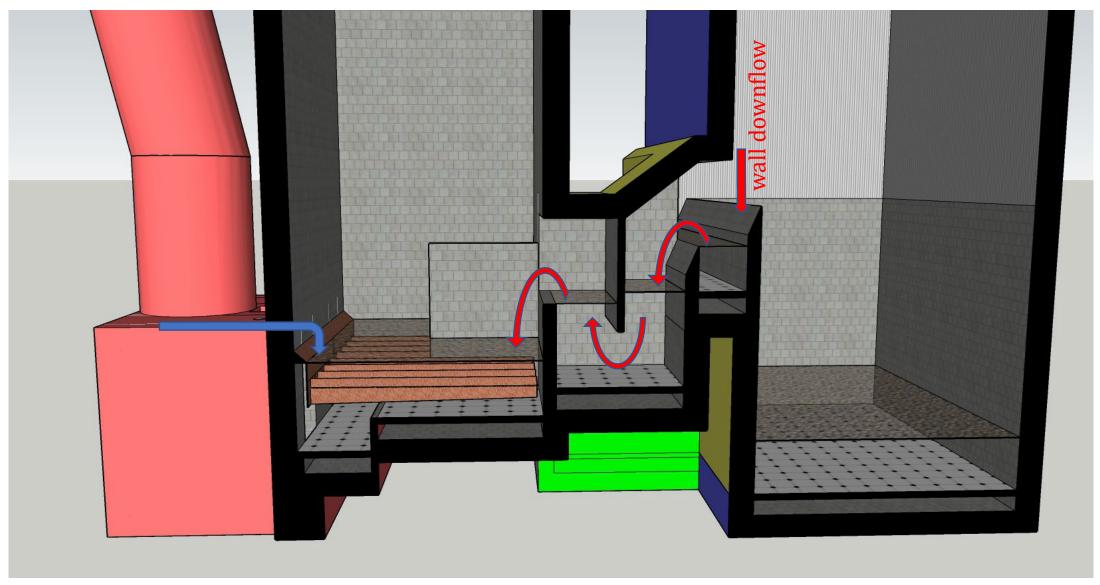
## 200 MW CLC-CFB boiler, 40 m high





Lyngfelt, A., Pallarés, D., Linderholm, C., Lind, F., Thunman, H., and Leckner, B., Achieving Adequate Circulation in Chemical-Looping Combustion – Design Proposal for a 200 MW<sub>th</sub> CLC Boiler, *Energy & Fuels* 36:17 (2022) 9588–9615

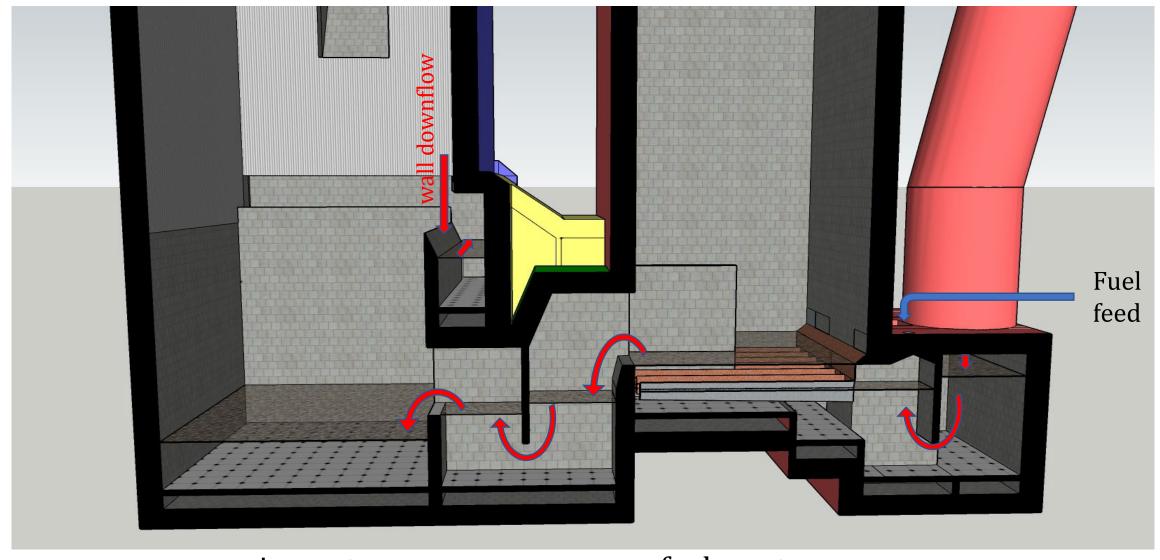
# Loopseal leading from air reactor to fuel reactor



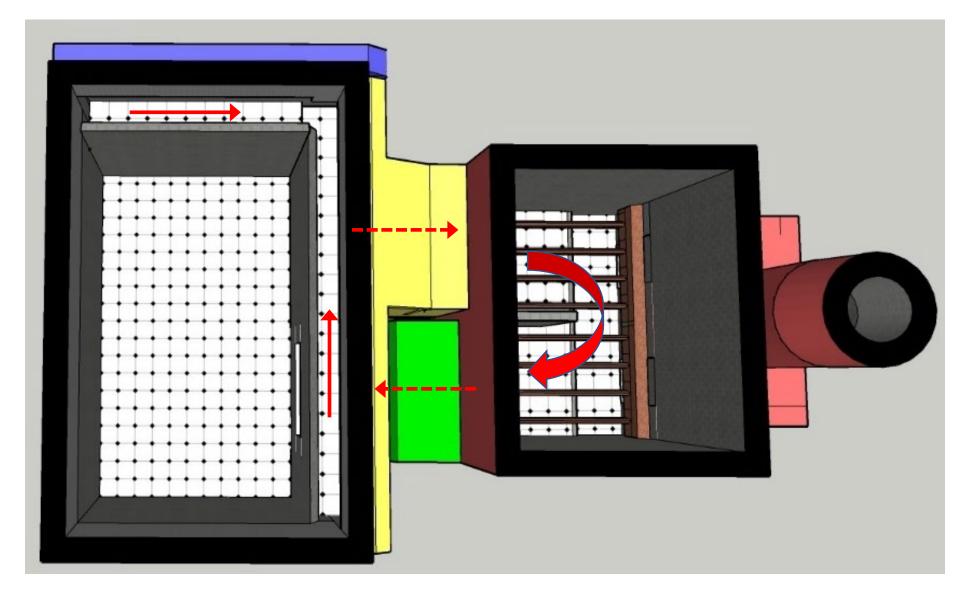
fuel reactor air reactor

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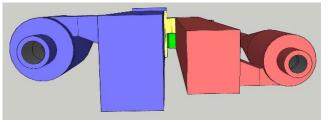
# Loopseal leading back from fuel reactor to airfuel reactor



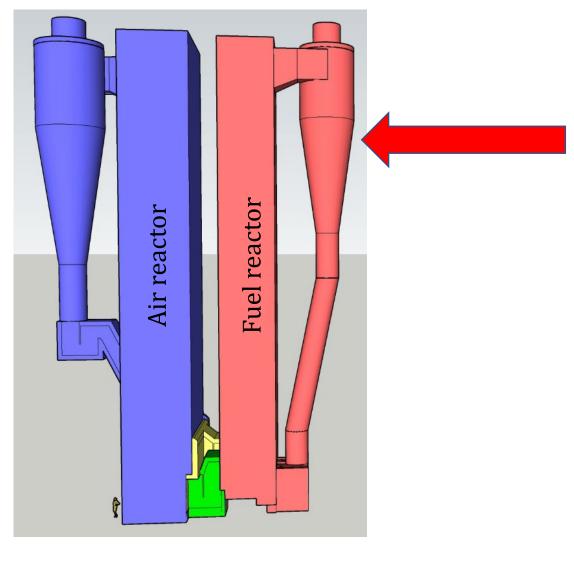
air reactor fuel reactor



air reactor



fuel reactor



200 MW CLC-CFB, added cost of Fuel Reactor: 1500 m<sup>2</sup> insulated wall

at 2000 €/m<sup>2</sup>

>>> 3 M€

or

0.3 M€/year

capture: 0.4 Mt CO<sub>2</sub>/year

cost of fuel reactor: 0.75 €/t CO<sub>2</sub>

Cost of post-combustion CO<sub>2</sub> capture:

•	_
bia	cost
-0 - 9	

Type of cost	estimatio €/tonne (	<i>y</i>	Efficiency penalty, %	
CO <sub>2</sub> compression	10	10	3	
Oxy-polishing	6.5	4-9	0.5	
Boiler cost	1	0.1-2.3	-	
Oxygen carrier	2	1.3-4	-	
Steam and hot CO <sub>2</sub> fluidization	0.8	0.8	0.8	
Fuel grinding	0.2	0.2	0.1	
Lower air ratio	-0.5	-0.5	-0.5	
<u>Total</u>	<u>20</u>	<u> 15.9-25.8</u>	3.9	
		small cost		

30

# 3) Purification of CO2 stream

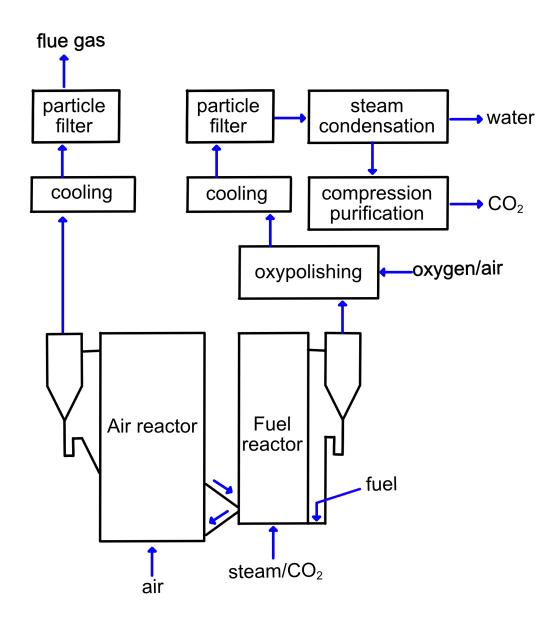


Table 2. Required purity of CO<sub>2</sub>. [69, 70]

Component	ppm
Water, H <sub>2</sub> O	≤30
Oxygen, O <sub>2</sub>	(≤10)
Sulphur oxides, SO <sub>x</sub>	≤10
Nitric oxide/nitrogen dioxide, NO <sub>x</sub>	≤10
Hydrogen sulphide, H <sub>2</sub> S	≤9
Carbon monoxide, CO	≤100
Amine	≤10
Ammonia, NH <sub>3</sub>	≤10
Hydrogen, H <sub>2</sub>	≤50
Formaldehyde	≤20
Acetaldehyde	≤20
Mercury	≤0.03
Cadmium + Thalium (sum)	≤0.03

#### **Measures for purification**

#### 1) Elimination of in-leakage

Downstream costs for removal of air ingress are very high.

Should not be a major technical issue to assure no, or very low, air ingress.

- Construction measures to assure no inleakage
  - Moving joints can use bellow seals and barrier gas (CO<sub>2</sub>)
  - Measures to seal discharge of fly-ashes
- Strict protocols for avoiding mistakes leading to air ingress
- Careful monitoring of gas purity, to detect and address any inleakage

#### 2) Removal of SO<sub>2</sub>

Any SO<sub>2</sub> present must be removed by wet flue gas desulphurization. Can be done in connection with water removal. Concentrated stream lowers costs, whereas need for high purity increases costs.

#### 3) Removal of NO<sub>x</sub>

#### Likely not needed:

- Partly reduced oxygen carrier ilmenite is efficient in reducing NO.
- Only way of NO formation is by oxidation fuel nitrogen by oxygen carrier.
- Equilibrium NO concentration in fuel reactor below 0.001 ppm

#### If needed:

- Conventional Selective Catalytic NOx Reduction.
  - High reduction not possible
  - Incoming NO needs to be low
- Co-removal of NO and SO<sub>2</sub>, at pressure, e.g. 30 bar.
  - Oxygen must be present
  - Deep reduction not possible, incoming NO must be low
  - Not commercial technology
- Addition of Cl<sub>2</sub>O, to the co-removal system
  - Deeper reduction possible
  - Not commercial technology
- Distillation of CO<sub>2</sub>

#### 4) Removal of O<sub>2</sub>

Catalytic combustion

- at high temperature with CH<sub>4</sub>
- at lower temperature with H<sub>2</sub>

#### 5a) Compression with single flash separation

With flash separation compounds of low solubility, e.g.  $N_2$ , NO,  $O_2$ , can be partly removed, depending on pressure.

Could be sufficient, if concentrations of gases that need deep reduction is low enough. Power need 2.9 - 3.8% of fuel heating value (coal),

#### 5b) Compression with cryogenic distillation

Remove gases with low solubility in  $CO_2$  to ppm levels. Removal steps 3) NO and 4)  $O_2$  not needed. Power need 7% of fuel heating value (coal) Necessary if NO cannot be lowered enough in 3)

#### 6) Drying of CO<sub>2</sub>

Water can be removed using molecular sieves or a dessicant, e.g. triethylene glycol

#### **Commercial CLC plant**

-

Three critical aspects that must have adequate solution

1) An oxygen carrier that works  $\square$ 

2) Adequate circulation  $\square$ 

3) Downstream treatment of gas from fuel reactor to achieve a  $CO_2$  that fulfills purity requirements for transportation/ storage

# **Chemical Looping combustion (CLC)**

CLC boiler very similar to CFB boiler (=circulating fludized-bed boiler)

Highly concentrated CO<sub>2</sub> stream can be obtained at small added cost

Cost: 25-50% of competing technologies for solid fuels

- Eliminate/reduce emissions of SO<sub>2</sub> (coal)
- Eliminate/reduce emissions of NO<sub>x</sub> (coal and biomass)
- Eliminate/reduce problems with alkali ash components (biomass)

Steam Methane Reforming with CLC

■ Potential for lower cost than conventional SMR without CO<sub>2</sub> capture, i.e. *negative* capture cost



Thank you!